

**REMARKS**

This Preliminary Amendment cancels original claims 1 to 16, and adds new claims 17 to 34 in the underlying PCT Application No. PCT/DE03/02041. The new claims conform the claims to the U.S. Patent and Trademark Office rules and do not add new matter to the application.

In accordance with 37 C.F.R. § 1.125, the Substitute Specification (including the Abstract, but without the claims) contains no new matter. The amendments reflected in the Substitute Specification (including the Title and Abstract) are to conform the Specification and Abstract to U.S. Patent and Trademark Office rules or to correct informalities. As required by 37 C.F.R. § 1.121 and § 1.125, a Marked Up Version Of The Substitute Specification comparing the Specification of record and the Substitute Specification also accompanies this Preliminary Amendment. In the Marked Up Version, underlining indicates added text and "strike-throughs" and double-brackets indicate deleted text. Approval and entry of the Substitute Specification (including Abstract) is respectfully requested.

The underlying PCT Application No. PCT/DE03/02041 includes an International Search Report, dated September 18, 2003, a copy of which is included. The Search Report includes a list of documents that were considered by the Examiner in the underlying PCT application.

It is asserted that the subject matter of the present application is new, non-obvious, and useful. Prompt consideration and allowance of the application are respectfully requested.

Respectfully Submitted,  
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**CUSTOMER NO. 26646**

METHOD FOR MONITORING AT LEAST TWO ELECTROMAGNETIC VALVES  
OF AN INTERNAL COMBUSTION ENGINE IN A  
MOTOR VEHICLE IN PARTICULAR

~~Background Information~~

FIELD OF THE INVENTION

The present invention is directed to a method for monitoring  
at least two electromagnetic valves of an internal combustion  
5 engine in a motor vehicle in particular, an actual current  
being supplied to each valve independently of the other  
valves, and a setpoint current being defined for each valve.  
The present invention also relates to a corresponding device  
for monitoring at least two electromagnetic valves. The  
10 present invention also relates to all applications in which  
the valves mentioned above are replaced by any other electric  
consumers of the internal combustion engine.

BACKGROUND INFORMATION

15 ~~DE~~German patent document no. 43 28 719 ~~At describes~~ discusses  
the detection and analysis of the current flowing through an  
electric consumer. A fault in the consumer is detectable by  
comparison with predetermined setpoint values.

20 If ~~the known~~ such a device is to be used with a plurality of  
consumers, a corresponding plurality of individual analyses is  
required. This may entails significant expenditure.

~~The~~ SUMMARY OF THE INVENTION

25 An object of the exemplary embodiment and/or exemplary method  
of the present invention is to create a method of the type

MARKED UP VERSION OF  
SUBSTITUTE SPECIFICATION

EL803886569us

defined at the outset that requires only minor expenditure even for a large number of valves.

#### ~~Object and Advantages of the Invention~~

5 In a method of the type ~~defined in the preamble~~described herein, this object ~~is~~may be achieved according to the exemplary embodiment and/or exemplary method of the present invention by determining a total actual current supplied to  
10 the valves, by adding the setpoint currents to yield a total setpoint current, by comparing the total setpoint current to the total actual current, and by using the result of the comparison to monitor the valves and/or their interconnection.

15 Thus the analysis is no longer performed individually for each consumer, as is the case in the related art, but instead all the valves are analyzed together. This is done by determining the total actual current and adding the setpoint currents together to yield the total setpoint current. These total  
20 currents are then compared according to the exemplary embodiment and/or exemplary method of the present invention. This results in the significant advantage of an extensive simplification of the entire method and greatly reduced monitoring complexity.

25 Essentially all the current supplied to a certain valve may be included in the monitoring. This permits particularly accurate and thus reliable monitoring.

30 In a first advantageous exemplary embodiment of the present invention, the actual currents supplied to the valves are measured by at least two measuring devices and added to yield the total actual current. Thus the actual currents measured by the two measuring devices are added up here.

In a second advantageous exemplary embodiment of the present invention, the actual currents supplied to the valves are measured by a single measuring device and used further as the total actual current. In this case, there is only one measuring device that measures the total actual current directly. It is apparent that this results in less expenditure for components and also omits the addition of measured actual currents.

It is particularly advantageous if a holding current with which the particular valve is held in an end position in a stable manner is used as the actual current. This further simplifies the entire monitoring procedure without any significant loss of accuracy.

It is also advantageous if a quenching current is used as the actual current, this quenching current resulting from the electric energy remaining in the valve after shutdown of the holding current. The quenching current is thus a feedback current, so that there is also monitoring in this regard.

In an advantageous further refinement of the exemplary embodiment and/or exemplary method of the present invention, chronological successive measurements and comparisons are used to detect a faulty valve from the point in time of occurrence of the difference. ~~It is thus possible,~~ with the exemplary method according to the present invention ~~to detect~~ not only may a fault be detected as such but it may also ~~to be~~ deduced that the valve is faulty.

In addition, the present invention is implemented by a computer program having program commands suitable for execution of the exemplary method according to the present invention when the computer program is running on a computer. The same thing is also true of a digital memory medium with a

computer program having program commands suitable for  
executing the exemplary method according to the present  
invention.

5 Other features, ~~possible applications, and advantages of the~~  
exemplary embodiment and/or exemplary method of the present  
invention are derived from the following description of  
exemplary embodiments and methods of the present invention,  
which are depicted in the drawing. ~~All described or depicted~~  
10 ~~features, either alone or in any combination, form the object~~  
~~of the present invention, regardless of how they are~~  
~~formulated in the patent claims or their back-reference and~~  
~~independently of their formulation and/or depiction in the~~  
~~description and/or in the drawing.~~

15 Drawing

~~Figure 1—drawings and/or otherwise described herein.~~

20 BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 shows a schematic block diagram of a first exemplary  
embodiment of a device according to the present invention for  
monitoring at least two electromagnetic valves of an internal  
combustion engine<sub>7</sub>.

25 Figure 2—\_shows a schematic wiring diagram for one of the  
electromagnetic valves of Figure 1, showing the current flow  
in four successive time ranges<sub>7</sub>.

30 Figure 3—\_shows a schematic time chart of the current across  
one of the electromagnetic valves of Figure 1 in the four time  
ranges<sub>7</sub>.

Figure 4—\_shows two schematic time charts of currents over two electromagnetic valves of Figure 1 in the four time ranges7\_.

5 Figure 5—\_shows a schematic block diagram of a second exemplary embodiment of a device according to the present invention for monitoring at least two electromagnetic valves of an internal combustion engine, ~~and~~.

10 Figure 6—\_shows two schematic time charts of currents over two electromagnetic valves from Figure 5.

~~Description of the Exemplary Embodiments~~

DETAILED DESCRIPTION

15 Figure 1 shows a device 10 for monitoring at least two electromagnetic valves 11, 12. Electromagnetic valves 11, 12 are provided for use in an internal combustion engine in a motor vehicle in particular.

20 It is pointed out explicitly that instead of valves 11, 12, the following description may also apply to any other electric consumers of the internal combustion engine. In addition, it is pointed out that the following description may be applied not only to two valves 11, 12 shown here, but device 10 may  
25 also be used for any plurality of valves, i.e., consumers, through appropriate expansions.

Two d.c. converters 13, 14 are provided for supplying power to valves 11, 12. D.c. converter 13 is suitable for generating a  
30 booster current on an electric line 15. Accordingly, d.c. converter 14 is suitable for generating a holding current on an electric line 16. The booster current is greater than the holding current.

A measuring device for measuring the booster current and another for the holding current are interconnected in lines 15, 16. The actual currents measured by measuring devices 17, 18 are sent to a control unit 19.

5

An output stage 20, via which the current flow through valves 11, 12 is controlled, is provided between meters 17, 18 and valves 11, 12. This control is provided via control unit 19. The function of output stage 20, its control, and the current flow generated by it over valve 11 are explained in greater detail below with reference to Figure 2. The explanation given there also pertains accordingly to the current flow through valve 12 and the current flow through any additional valve.

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Figure 2 shows lines 15, 16 coming from two d.c. converters 13, 14. Line 16 is connected via a diode D1, which is connected in the flow direction, to one of the two terminals of electromagnetic valve 11. The other terminal of electromagnetic valve 11 is connected via a diode D2, which is also connected in the flow direction, to line 15. The cathodes of both diodes D1, D2 are interconnected via switch S1. The anode of diode D2 is connected to ground across a switch S2.

20

Depending on the switch positions of two switches S1, S2, there is a different current flow across valve 11. Four different switch positions resulting in four different current flows in four successive time ranges a, b, c, d may be set using two switches S1, S2. The positions of two switches S1, S2 are controlled by control unit 19 as already mentioned.

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Figure 3 shows current  $I_{MV}$  across electromagnetic valve 11 as a function of time. In particular, four time ranges a, b, c, d resulting from the four adjustable switch settings of two switches S1, S2 are shown in Figure 3.

35

In first time range a, both switches S1, S2 are closed. This yields a current flow a, as depicted in Figure 2 and designated accordingly as "a." The booster current generated by d.c. converter 13 flows across valve 11. This current  $I_{MV}$  increases up to a final value.

In second time range b, which follows time range a, switch S1 is closed and switch S2 is opened. This yields a current flow as depicted in Figure 2 and designated accordingly as "b." This current flow is ~~known~~referred to as a free-running state. This means that at least a portion of the electric energy contained in electromagnetic valve 11 is dissipated via this free-running state. Accordingly, current  $I_{MV}$  declines in time range b according to Figure 3.

Switch S1 is opened in time range c and switch S2 is closed. This yields a current flow like that depicted in Figure 2, where it is designated accordingly as "c." The holding current generated by d.c. converter 14 in time range c is sent to valve 11. This holding current is selected so that the end position reached by valve 11 on the basis of the booster current does not change.

Both switches S1, S2 are open in time range d which follows time range c. This yields a current flow like that depicted in Figure 2 and designated accordingly as "d." This current flow constitutes quenching of electromagnetic valve 11. This means that the energy contained in electromagnetic valve 11 is completely dissipated to 0. Current  $I_{MV}$  then issuing from valve 11 flows across diode D2 to d.c. converter 13 in time range d. Thus a feedback current flows, this current being measurable by measuring device 17 in the same way as the booster current flowing in the direction toward valve 11.



As mentioned previously, the actual current flowing to valves 11, 12 is measured by measuring devices 17, 18, and the measurement result is sent to control unit 19. Control unit 19 adds the currents measured by measuring devices 17, 18 to yield a total actual current  $I_{addactual}$ . This is depicted in the top time chart in Figure 4.

In Figure 4 it is assumed that two valves 11, 12 each receive current  $I_{MV}$  depicted in Figure 3 in short intervals in succession. In the bottom time chart in Figure 4, these two currents  $I_{MV}$  are depicted as setpoint currents  $I_{11}$ ,  $I_{12}$ . The time interval between these two setpoint currents  $I_{11}$ ,  $I_{12}$  is characterized as time period  $T$ .

Two setpoint currents  $I_{11}$ ,  $I_{12}$  result from the fact that switches  $S1$ ,  $S2$  of output stage 20 are triggered by control unit 19 in such a way that essentially setpoint currents  $I_{11}$ ,  $I_{12}$  mentioned above will have to flow across valves 11, 12. However, there is the possibility that because of some malfunction, setpoint currents  $I_{11}$ ,  $I_{12}$  might not actually flow or at least might be modified.

Such faults may be recognized by control unit 19 as follows:

As mentioned above, switches  $S1$ ,  $S2$  of output stage 20 are triggered by control unit 19, so ~~it is possible for control unit 19 to may~~ compute setpoint currents  $I_{11}$ ,  $I_{12}$  and in particular their plot over time. ~~It is thus also possible for~~ Control unit 19 ~~to may also~~ add the calculated setpoint currents  $I_{11}$ ,  $I_{12}$ . This yields total setpoint current  $I_{addsetpoint}$  depicted in the bottom time chart in Figure 4.

As already explained previously, control unit 19 also determines total actual current  $I_{addactual}$ . This total actual current  $I_{addactual}$  is depicted in the top time chart in Figure 4.

~~It is thus possible in~~In an additional step for control unit 19 ~~to compare,~~ total actual current  $I_{\text{addactual}}$  may be compared with expected total setpoint current  $I_{\text{addsetpoint}}$ .

5 If this comparison does not reveal any deviation between two total currents, this means that there is no fault. Setpoint currents  $I_{11}$ ,  $I_{12}$  calculated by control unit 19 thus in fact flow across valves 11, 12. This fault-free case occurs when total actual current  $I_{\text{addactual}}$  corresponds to the solid line  
10 according to the top time chart in Figure 4.

However, if total actual current  $I_{\text{addactual}}$  deviates from total setpoint current  $I_{\text{addsetpoint}}$ , this means that there is a fault in device 10 in Figure 1. Two fault cases are described below as  
15 examples on the basis of the top time chart in Figure 4.

If the total actual current has a curve like that shown with a dotted line for faulty total current  $I_{F1}$  in the top time chart in Figure 4, the comparison of this faulty total current  $I_{F1}$   
20 with total setpoint current  $I_{\text{addsetpoint}}$  will show a deviation. From corresponding computations, control unit 19 may then determine that the deviation is based on a faulty current for valve 12. This results from the fact that setpoint current  $I_{11}$  for valve 11 is completely contained in faulty total current  
25  $I_{F1}$ , but there are no components of setpoint current  $I_{12}$  for valve 12. According to the top time chart in Figure 4, these components include the booster current and the following free-running state for valve 12.

30 If total actual current  $I_{\text{addactual}}$  has a curve like that shown as an example as faulty total current  $I_{F2}$  in the top time chart in Figure 4, this in turn represents a deviation of total current  $I_{F2}$  from total setpoint current  $I_{\text{addsetpoint}}$ . Control unit 19 thus again recognizes a fault in device 10 of Figure 1.

On the basis of the time conditions of the deviation of the faulty total current, ~~it is possible for control unit 19~~ may not only ~~to~~ recognize a fault as such but may also ~~to~~ localize the fault more precisely. Control unit 19 is able to deduce on the basis of the curve of faulty total current  $I_{F2}$  that the booster current and free-running state of both valves 11, 12 were correct. However, the deviation in faulty total current  $I_{F2}$  occurs in the range of the holding currents for two valves 11, 12. ~~It is thus theoretically possible that either the~~ holding current for valve 11 or the holding current for valve 12 may have a dip that results in the deviation in faulty current  $I_{F2}$ . There is a greater probability that the holding current has been ended too soon for valve 11 and that this has resulted in the deviation in faulty total current  $I_{F2}$  from expected total setpoint current  $I_{addsetpoint}$ .

Thus on the whole, control unit 19 adds the currents measured by measuring devices 17, 18 to yield a total actual current  $I_{addactual}$ . In addition, control unit 19 determines as a function of the triggering of switches S1, S2 of output stage 20 total setpoint current  $I_{addsetpoint}$  that would have to be present on the basis of the aforementioned triggering of switches S1, S2. Control unit 19 then compares total actual current  $I_{addactual}$  and total setpoint current  $I_{addsetpoint}$ . If there is no deviation between them, device 10 is functioning without fault. If there is a deviation, this means that there is a fault in device 10. Control unit 19 is able to localize the fault of device 10 more precisely, in particular to limit it to one of valves 11, 12, from the time conditions, in particular from the point in time of occurrence of a deviation in total actual current  $I_{addactual}$  from total setpoint current  $I_{addsetpoint}$ .

Figure 5 corresponds largely to Figure 1. For this reason, the same reference numerals also have the same meanings. The difference between Figure 1 and Figure 5 is that d.c.

converter 14, measuring device 18, diodes D1 and corresponding electric line 16 are no longer present. Only single measuring device 17 remains and measures the current generated by single d.c. converter 13.

5  
Remaining d.c. converter 13 is no longer provided for generating the booster current but instead is provided for generating the holding current. To do so, two switches S1, S2 are either closed simultaneously so that the holding current  
10 flows across both valves 11, 12 or switch S1 is closed and switch S2 is opened so that the holding current is quenched.

As in Figure 4, it is also assumed in Figure 6 that both valves 11, 12 receive a current one after the other in short  
15 intervals. This is depicted by two setpoint currents  $I_{11}$ ,  $I_{12}$  in the bottom time chart in Figure 6, these currents being generated by the triggering of switches S1, S2 as mentioned above, and their time interval being again referred to as time period T. Addition of two setpoint currents  $I_{11}$ ,  $I_{12}$  yields  
20 total setpoint current  $I_{\text{addsetpoint}}$  of Figure 6.

A total actual current  $I_{\text{actual}}$  is plotted in the top time chart in Figure 6. In contrast with Figure 4, where total actual current  $I_{\text{addactual}}$  is obtained by adding two currents generated by  
25 two d.c. converters 13, 14 and flowing across two measuring devices 17, 18, total actual current  $I_{\text{actual}}$  in Figure 6 is generated directly by d.c. converter 13 and measured by a single measuring device 17. Thus there is no adding of the actual currents in Figure 6 or in Figure 4.

30  
Total actual current  $I_{\text{actual}}$  is compared with total setpoint current  $I_{\text{addsetpoint}}$ . If this comparison does not yield any deviations, this means that there is no fault. However, if there is a deviation, this indicates that there is a fault.

A faulty current  $I_{F1}$ , which does not match total setpoint current  $I_{addsetpoint}$  of the lower time chart in Figure 6, is indicated in the top time chart in Figure 6. A fault may be deduced in conjunction with the current flowing across valve 12 on the basis of the curve of this faulty current  $I_{F1}$  and its comparison with total setpoint current  $I_{addsetpoint}$ .

~~Abstract~~ ABSTRACT OF THE DISCLOSURE

A device for monitoring at least two electromagnetic valves  
(11, 12) of an internal combustion engine in a motor vehicle  
~~in particular is described.~~ An actual current that is  
5 independent of the other valves (12) may be supplied to each  
valve (11). A setpoint current ( ~~$I_{11}$ ,  $I_{12}$~~ ) is preselected for  
each valve (11, 12). Measuring devices (17, 18) are provided  
for measuring the actual currents supplied to the valves (11,  
12). A control unit (19) ~~is provided and~~ is used to add the  
10 measured actual currents to yield a total actual current  
( ~~$I_{\text{addactual}}$~~ ). Due to the control unit (19), the setpoint currents  
( ~~$I_{11}$ ,  $I_{12}$~~ ) are added to yield a total setpoint current  
( ~~$I_{\text{addsetpoint}}$~~ ) and compared to the total actual current ( ~~$I_{\text{addactual}}$~~ ).  
This comparison is used by the control unit (19) for  
15 monitoring the valves (11, 12) and/or their interconnections.

~~Figure 1~~